

**ROCHESTER INSTITUTE OF TECHNOLOGY
MICROELECTRONIC ENGINEERING**

Basic Analog Electronic Circuits Using Operational Amplifiers

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5-14-2020 Basic_Analog_Circuits.pptx

OUTLINE

Introduction
Op Amp
Comparator
Bistable Multivibrator
RC Oscillator
RC Integrator
Peak Detector
Switched Capacitor Amplifier
Capacitors
Design Examples
References
Homework



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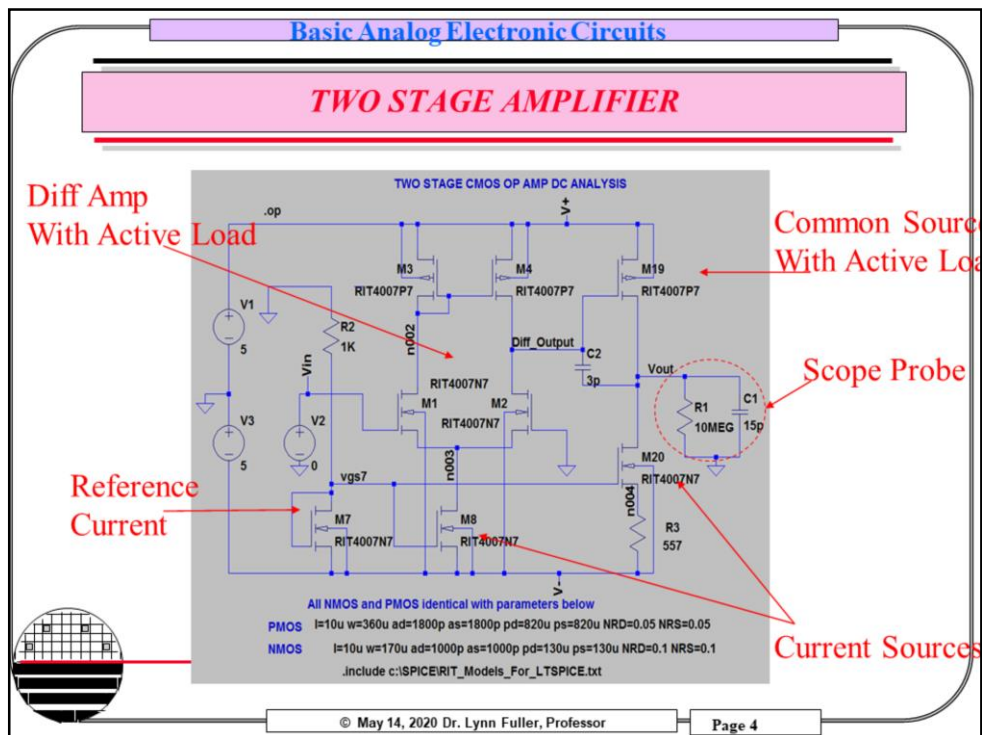
INTRODUCTION

Analog electronic circuits are different from digital circuits in that the signals are expected to have any value rather than two discrete values. **Primitive** analog components include the diode, mosfet, BJT, resistor, capacitor, etc,. Analog circuit **building blocks** include single stage amplifiers, differential amplifiers, constant current sources, voltage references, etc. **Basic** analog electronic circuits include the operational amplifier, inverting amplifier, non-inverting amplifier, integrator, bistable multivibrator, peak detector, comparator, RC oscillator, etc. **Mixed-mode** analog integrated circuits include D-to-A, A-to-D, etc.

This document will introduce some **Basic** analog electronic circuits using operational amplifiers.

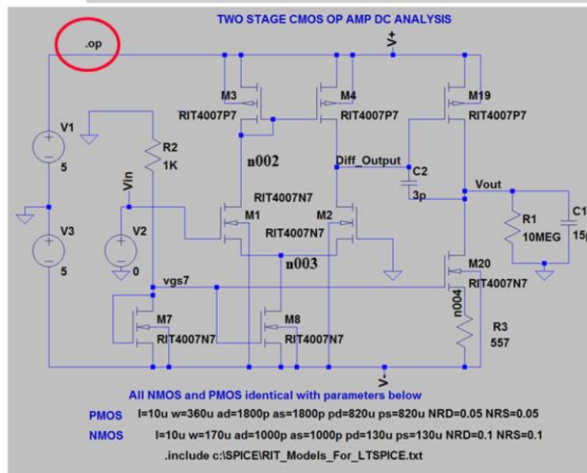


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This is the CMOS op amp that we will build in lab. Look carefully at the schematic and identify the current sources, reference current, differential amplifier, active loads, common source 2nd stage with active load and scope probe. (note: MEG works in spice but M is milli and m is also milli) Note the current source for the 2nd stage is different than M8 in that R3 will make the current smaller.

DC ANALYSIS



Some results:

$$I_{ref} = I(R2) = 1.81mA$$

$$I_{EE} = I(M8) = 1.77mA$$

$$I(M1) = I(M2) = 0.884mA$$

$$I(M20) = I(R3) = 0.904mA$$

$$V_{gs7} = -1.81 + 5 = 3.19V$$

$$V(Dif_output) = 1.89$$



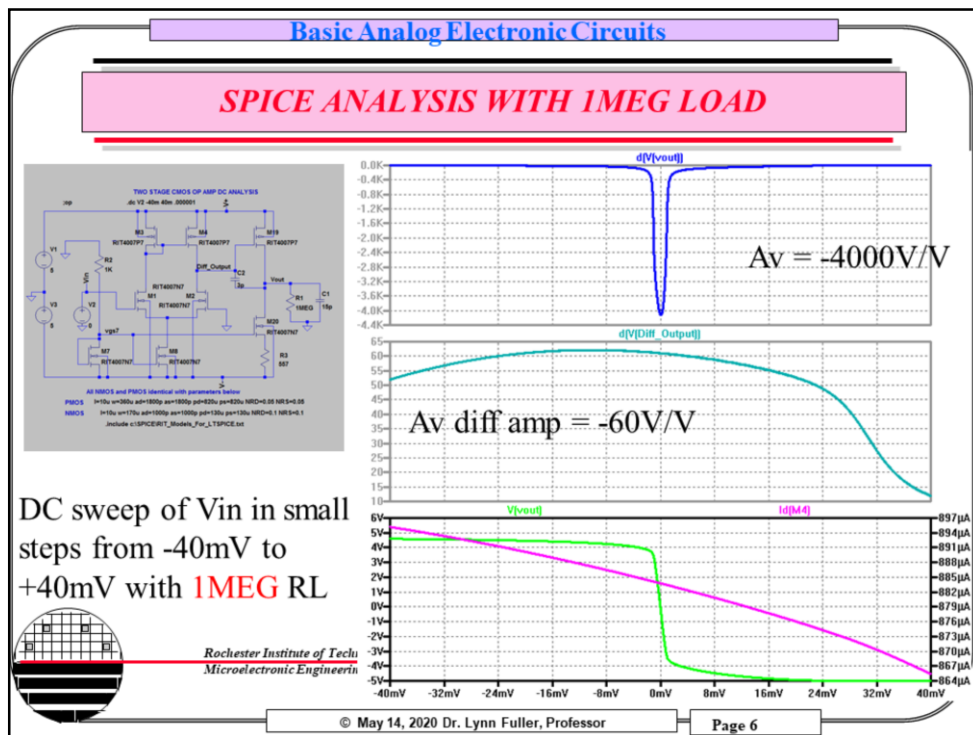
.op - No plot is displayed but a list of all DC node voltages and branch currents is given

(see next page)

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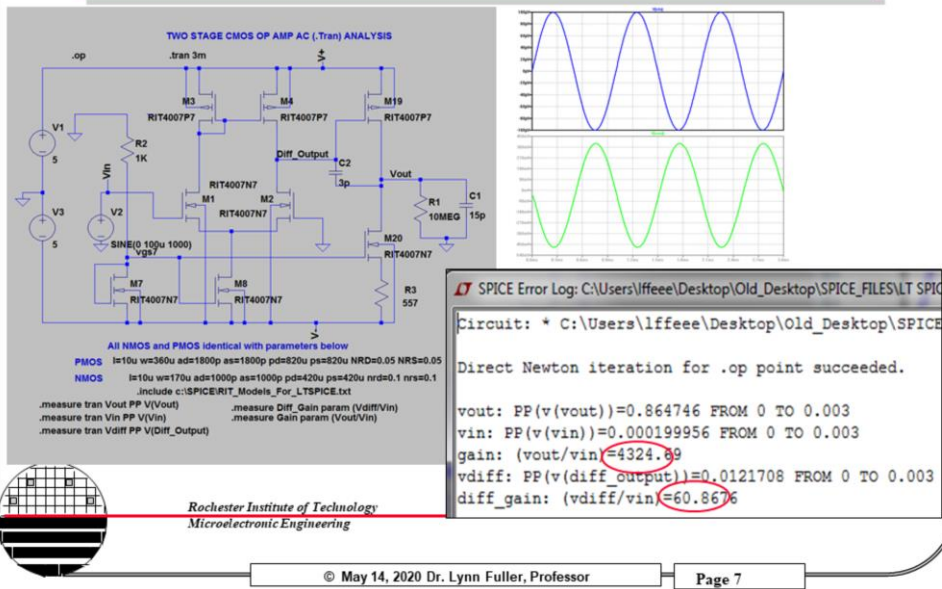
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Start with the DC analysis. In LTSPICE the .op command does the DC analysis and lists all the node voltages and branch currents in a table after running the simulation. Some of the results in the table are given here. The reference current $I(R2)$ is 1.81 mA and is matched with the current source $I_{M8} = I_{EE} = 1.77mA$. I_{EE} splits in half for the diff amp transistors giving 0.884 mA each. The current in the 2nd stage is 0.9mA. The DC output offset voltage is 40mV which is close to zero as desired.



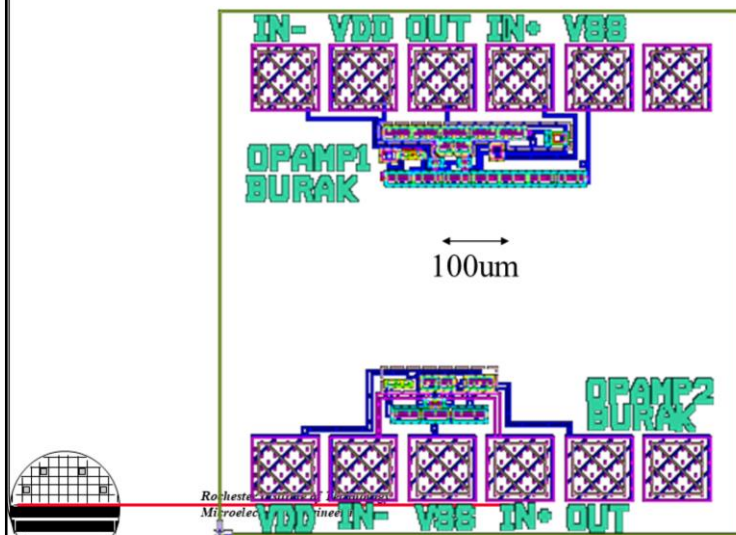
One way to get the voltage gain (the other is to input sine wave) is to do a DC sweep near zero volts. In this example we sweep from -40mV to $+40\text{mV}$ in small steps. The output voltage is shown in green. The derivative of the green plot is shown in dark blue in the top plot plane and is the overall voltage gain. The derivative of the differential amp stage output voltage is the gain of the diff amp shown in the middle plot plane. The maximum overall gain is $\sim 4000\text{V/V}$ and for the diff amp is $\sim 60\text{V/V}$.

SINE INPUT – SPICE TRAN. ANALYSIS – 10MEG LOAD



Similar results are found for sinusoidal input.

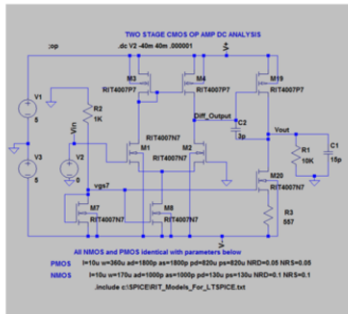
OPERATIONAL AMPLIFIER LAYOUT



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This shows two versions of the layout of the op amp shown on the previous few pages. The upper design is based on $L=2\mu\text{m}$. The lower design is a $L=1\mu\text{m}$ design. They should both work but the larger one always works when made by RIT students.

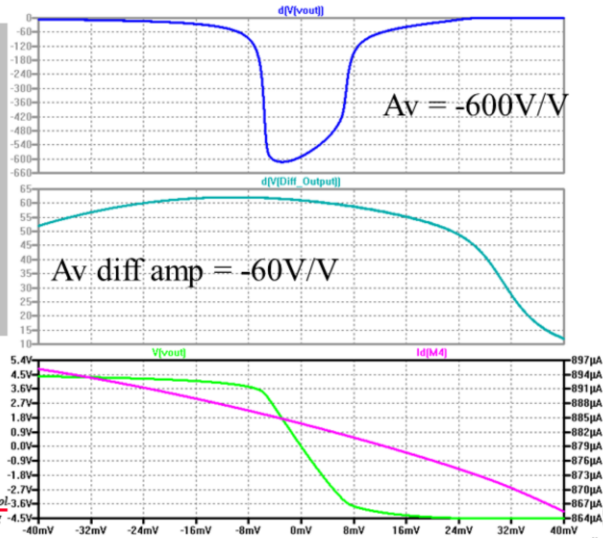
SPICE ANALYSIS WITH 10K LOAD



DC sweep of V_{in} in small steps from -40mV to +40mV with

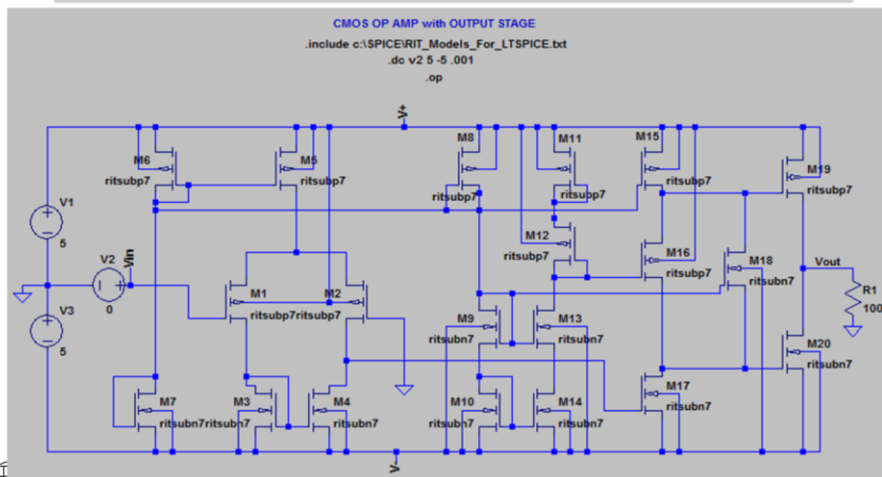


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With a 10K load the voltage gain drops from ~4000V/V to ~600V/V. Obviously this amplifier has little ability to output current to loads less than 1MEG ohm.

CMOS OP AMP WITH OUTPUT STAGE



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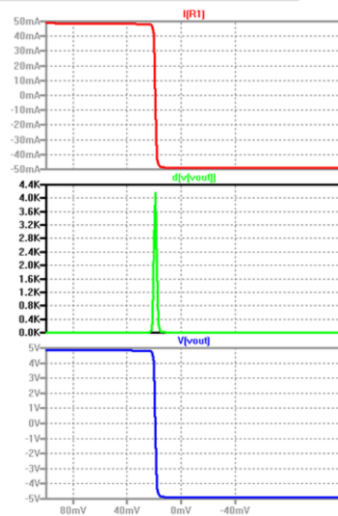
LTSPICE for CMOS op amp with output stage to drive loads of 100 ohms.

CMOS OP AMP WITH OUTPUT STAGE

Note: R1 is the load resistor = 100 ohms

The voltage gain is still 4000 V/V
and the current is +/- 50mA

Not possible with the two stage Op Amp



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A few extra transistors allows the op amp to drive 100 ohm loads.

OPERATIONAL AMPLIFIERS

The 741 Op Amp is a general purpose bipolar integrated circuit that has input bias current of 80nA, and input voltage of ± 15 volts @ supply maximum of ± 18 volts. The output voltage can not go all the way to the + and - supply voltage. At a minimum supply of ± 5 volts the output voltage can go ~ 6 volts p-p.

The newer Op Amps have rail-rail output swing and supply voltages as low as ± 1.5 volts. The MOSFET input bias currents are ~ 1 pA. The NJU7031 is an example of this type of Op Amp.



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Please read.

LOW VOLTAGE, RAIL-TO-RAIL OP AMP

JRC

NJU7031/32/34

LOW VOLTAGE C-MOS OPERATIONAL AMPLIFIER

GENERAL DESCRIPTION

The NJU7031/32/34 are single, dual and quad single supply, low offset, output full swing C-MOS Operational Amplifiers. The wide operating voltage 3V to 16V, High slew rate 3.5V/ μ s and output full swing are suitable for fast signal processing amplifiers. Additionally, low input bias current 1pA, and single supply operation offer amplification of the very small signal around the ground level.

The NJU7031 has external offset null function.

FEATURES

- High Slew Rate 3.5V/ μ s
- Wide Operating Voltage +3V to +16V
- Output Voltage with full Swing $V_{OL}=9.98V$ typ. (@ $V_{CC}=10V$)
- Input Common Mode Voltage Range $V_{CM}=0V$ to 9V (@ $V_{CC}=10V$)
- Low Bias Current $I_B=1pA$ typ.
- Input Common Mode Voltage range includes ground.
- External Offset Null Adjustment (Only NJU7031)
- C-MOS Technology
- Package Outline
 - NJU7031 (single) DIP8, DMP8, SSOP8
 - NJU7032 (dual) DIP8, DMP8
 - NJU7034 (quad) DIP14, DMP14, SSOP14

PACKAGE OUTLINE



NJU7031D
NJU7032D



NJU7031M
NJU7032M



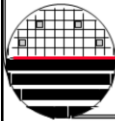
NJU7034D



NJU7034M

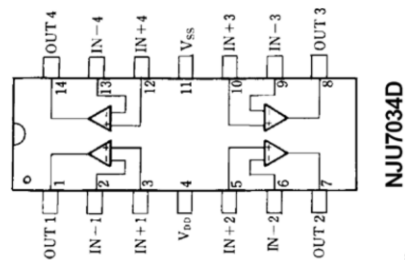
NJU7034V

1. 3 to 16 Volt operation
2. Rail to Rail input and output voltages
3. Low Input bias $\sim 1pA$
4. Output Current $\sim 1mA$
5. Unity Gain Bandwidth 1.5 MHz
6. Power Dissipation 1mA at 3 V = 3000uW



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New Japan Radio Co., Ltd.



NJU7034D

NJU703X OP AMP DATA SHEET

NJU7031/32/34

■ ABSOLUTE MAXIMUM RATINGS

(Ta=25°C)			
PARAMETER	SYMBOL	RATINGS	UNIT
Supply Voltage	V_{DD}	18	V
Differential Input Voltage	V_{ID}	± 18 (note 1)	V
Common Mode Input Voltage	V_{IC}	-0.3~18	V
Power Dissipation	P_D	(DIP14) 700 (DIP8) 500 (DMPS, 14) 300 (SSOP8, 14) 300	mW
Operating Temperature Range	T_{OP}	-40~+85	°C
Storage Temperature Range	T_{STG}	-40~+125	°C

(note 1) If the supply voltage (V_{DD}) is less than 18V, the input voltage must not over the V_{DD} level though 18V is limit specified.

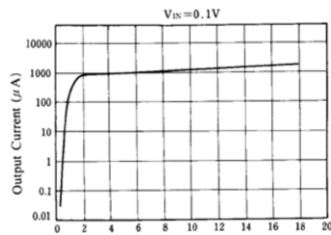
■ ELECTRICAL CHARACTERISTICS

(Ta=25°C, $V_{DD}=10$)					
PARAMETER	SYMBOL	TEST CONDITION	MIN.	TYP.	MAX. UNIT
Input Offset Voltage	V_{IO}	$R_L=50\Omega$	-	-	10 mV
Input Offset Current	I_{IO}		-	1	pA
Input Bias Current	I_{BI}		-	1	pA
Input Impedance	R_{ii}		-	1	TΩ
Large Signal Voltage Gain	A_v		80	95	dB
Input Common Mode Voltage Range	V_{CM}		0~9	-	V
Maximum Output Swing Voltage	V_{OM}	$R_L=1M\Omega$	9.80	9.98	V
Common Mode Rejection Ratio	CMR		60	75	dB
Supply Voltage Rejection Ratio	SVR		60	75	dB
Operating Current/Circuit	I_{OO}		-	1	mA/Cir
Slew Rate	SR		-	3.5	V/ μ s
Unity Gain Bandwidth	F_t	$A_v=40dB, C_L=10pF$	-	1.5	MHz

■ OFFSET ADJUSTMENT CIRCUIT (Only For NJU7031)

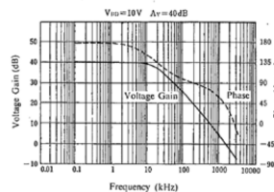
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Output Current vs. Operating Voltage

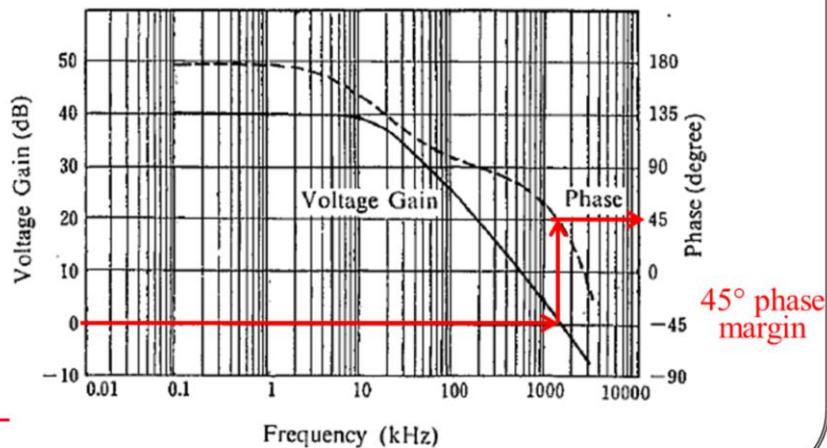


Operating Voltage (V)

Voltage Gain - Phase vs. Frequency



More from the data sheet.

PHASE MARGIN**Voltage Gain • Phase vs. Frequency** $V_{DD} = 10\text{ V}$ $A_V = 40\text{ dB}$ 

This is a plot of the voltage gain and phase vs Frequency for an inverting amplifier configuration with, R_f and R_{in} , to give a low frequency gain to 40 dB or 100 V/V.

LTC6078 OP AMP



LTC6078/LTC6079
Micropower Precision,
Dual/Quad CMOS
Rail-to-Rail Input/Output Amplifiers

FEATURES

- Maximum Offset Voltage of 25µV (25°C)
- Maximum Offset Drift of 0.7µV/°C
- Maximum Input Bias: 1pA (25°C)
50pA (±85°C)
- Micropower: 54µA per Amp
- 50dB CMRR (Min)
- 100dB PSRR (Min)
- Input Noise Voltage Density: 16nV/√Hz
- Rail-to-Rail Inputs and Outputs
- 2.7V to 5.5V Operation Voltage
- LTC6078 Available in 8-Lead MSOP and 10-Lead DFN Packages; LTC6079 Available in 10-Lead SSOP and DFN Packages

APPLICATIONS

- Photodiode Amplifier
- High Impedance Sensor Amplifier

DESCRIPTION

The LTC6078/LTC6079 are dual/quadruple, low offset, low noise operational amplifiers with low power consumption and rail-to-rail input/output swing. Input offset voltage is trimmed to less than 25µV and the CMOS inputs draw less than 50pA of bias current. The low offset drift, excellent CMRR, and high voltage gain make it a good choice for precision signal conditioning.

Each amplifier draws only 54µA current on a 3V supply. The micropower, rail-to-rail operation of the LTC6078/LTC6079 is well suited for portable instruments and single supply applications.

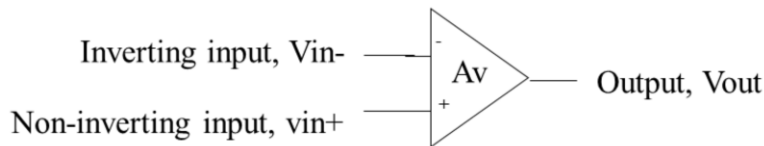
The LTC6078/LTC6079 are specified on power supply voltages of 3V and 5V from -40 to 125°C. The dual amplifier LTC6078 is available in 8-lead MSOP and 10-lead DFN packages. The quad amplifier LTC6079 is available in 10-lead SSOP and DFN packages.

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ELECTRICAL CHARACTERISTICS

The μ denotes the specifications which apply over the full operating temperature range. Otherwise specifications are at $T_A = 25^\circ\text{C}$. Test conditions are $V_S = 2.7\text{V}$ or 5V , $V_{IN} = 0\text{V}$ unless otherwise noted.

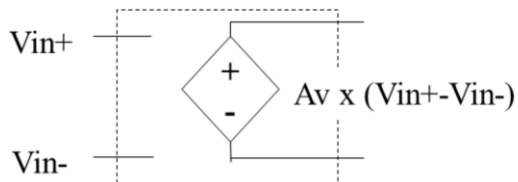
SYMBOL	PARAMETER	CONDITIONS	C, 1 SUPPLIES			5 SUPPLIES			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
V_{OS}	Offset Voltage (Note 1)	LTC6078/LTC6079/LTC6079A, LTC6078/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±7	±25		±7	±25	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±7	±25		±7	±25	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±20	±10		±20	±10	µV
I_{OS}	Input Offset Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
I_{B}	Input Bias Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±2.5	±1.0		±2.5	±1.0	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current Density (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage Density (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}	Input Noise Current (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
V_{IN}	Input Noise Voltage (Note 1)	LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
		LTC6078/LTC6079A, LTC6079/LTC6079A							µV
		$V_{IN} = 0\text{V}$ to 2.7V		±1.1	±1.1		±1.1	±1.1	µV
I_{N}									

THE IDEAL OPERATIONAL AMPLIFIER

The ideal operational amplifier has infinite input resistance, zero output resistance and very high voltage gain,

$$A_v = V_{out} / (V_{in+} - V_{in-}) = 10,000 \text{ V/V or more.}$$

The small signal equivalent circuit is shown



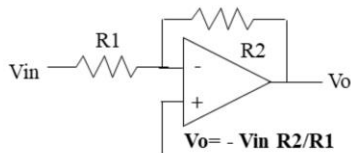
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These properties imply in zero current into either of the differential inputs because the input resistance is infinite.

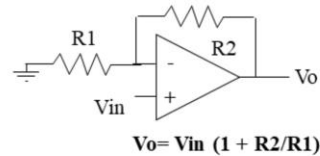
And very small voltage difference between the two inputs, (we say V_{in+} and V_{in-} are at virtually the same voltage). This is because if the output voltage is finite the input is output divided by the very high gain, resulting in a very small voltage difference input.

SOME BASIC ANALOG ELECTRONIC CIRCUITS

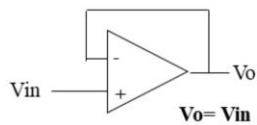
These circuits should be familiar:



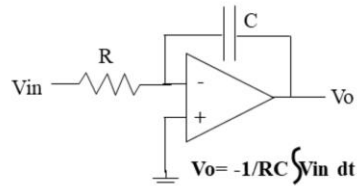
Inverting Amplifier



Non-Inverting Amplifier



Unity Gain Buffer

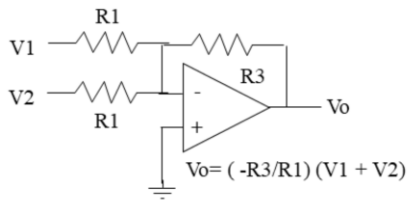


Integrator

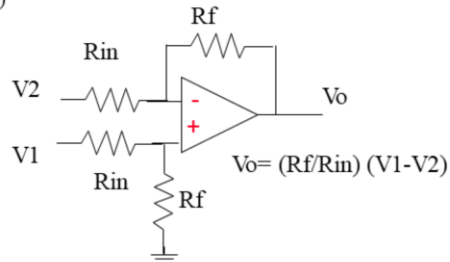


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These basic op amp circuits should be familiar. Let's apply ideal op amp fundamentals to the Inverting amplifier. V_{in+} and V_{in-} are virtually at the same voltage, virtual ground and ground. The current in R_1 is V_{in}/R_1 . With infinite input resistance the current in R_1 has to go through R_2 creating a voltage at V_o of $-I \times R_2$ which is equal to V_o . Combining these two equations we have $V_o/V_{in} = -R_2/R_1$ the inverting amplifier gain. You can apply these same concepts to derive the output equations for each of these circuits. Note the feedback connection always goes from V_o back to the inverting input.

SOME BASIC ANALOG ELECTRONIC CIRCUITS

Inverting Summer



Difference Amplifier



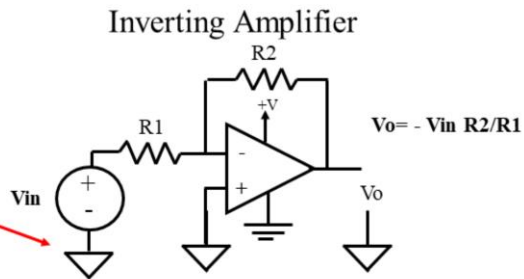
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Two more basic op amp circuits. You can use the concepts of the ideal op amp with other circuit analysis techniques to derive the equation for the output voltage. The concept of superposition for linear circuits can help with these two circuits. That is find V_{out} due to V_1 with V_2 equal to zero and add the result to V_{out} due to V_2 with V_1 equal to zero.

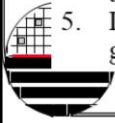
INVERTING AMPLIFIER SINGLE SUPPLY EXAMPLE



These Grounds are not the same



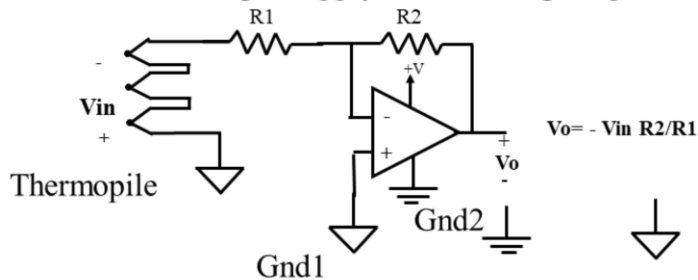
1. This is a DC and AC amplifier.
2. The input is referenced to the analog ground typically $\frac{1}{2}$ of +V
3. The output voltage is referenced to the virtual ground or to earth ground.
4. If using a scope to measure V_o the scope ground is earth ground. If the V_{in} is ac you can AC couple the scope.
5. If the input V_{in} is DC you can measure the output relative to the analog ground using a multimeter (not the oscilloscope)



Most op amp circuits use dual power supplies so that the input and output voltages are referenced to ground. However, it is sometimes useful to use a single supply instead of two. In the single supply case the input and outputs should be referenced to a voltage near $\frac{1}{2}$ of the single supply value. This requires careful consideration of grounds and analog signal grounds which are not the same for single supply op amp circuits.

INVERTING AMPLIFIER SINGLE SUPPLY EXAMPLE

Single Supply DC Inverting Amplifier



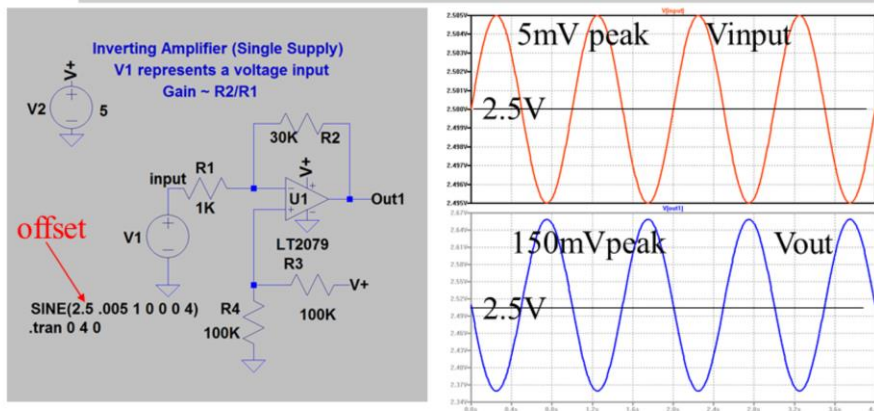
Gnd1 is analog ground $\sim 1/2$ of supply voltage. Vout can be taken relative to Gnd1 or Gnd2 however there is a $+V/2$ DC added to V_o if relative to Gnd2.



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This is an example of a single supply op amp inverting amplifier for a small DC input voltage from a thermopile, V_{in} . If you had a analog ground at a voltage at $1/2$ way between the $+V$ and ground the output voltage would be $1/2$ way between $+V$ and ground for no V_{in} . With V_{in} not zero V_{out} will be $-V_{in} (R_2/R_1)$ plus $V+/2$ volts.

INVERTING AMPLIFIER EXAMPLES



The two 100K resistors create an analog ground $\sim 1/2 V+$ the gain = $-R2/R1$, offset of $V+/2$ or analog ground

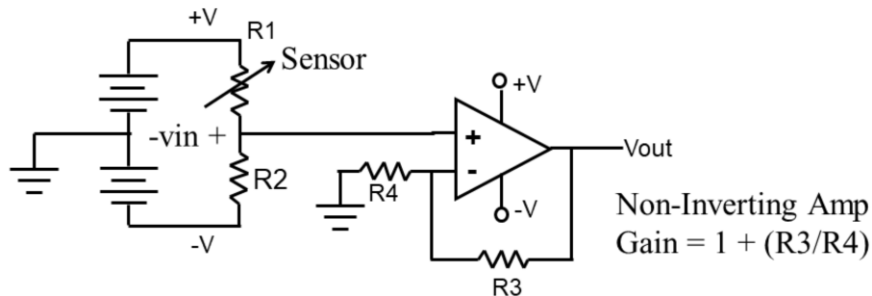


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This shows a single supply amplifier for a sinusoidal input with a DC offset equal to the analog ground. In this case $V+$ divided by two. The output voltage is a sinusoid on a DC offset of $V+/2$. That is $5/2 = 2.5$ volts.

SINGLE RESISTOR SENSOR AMPLIFIER DESIGN

If the sensor resistor $R1$ increases in response to some physical change vin will decrease slightly. The amplifier has a voltage gain of $\text{Gain} = 1 + (R3/R4)$ with infinite input resistance.

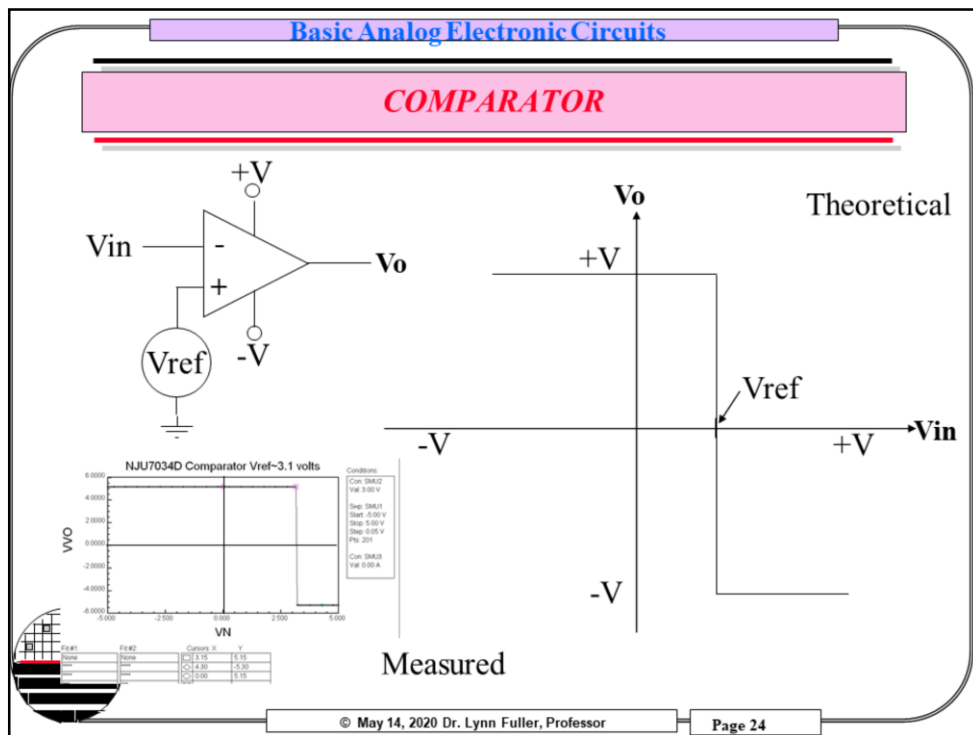


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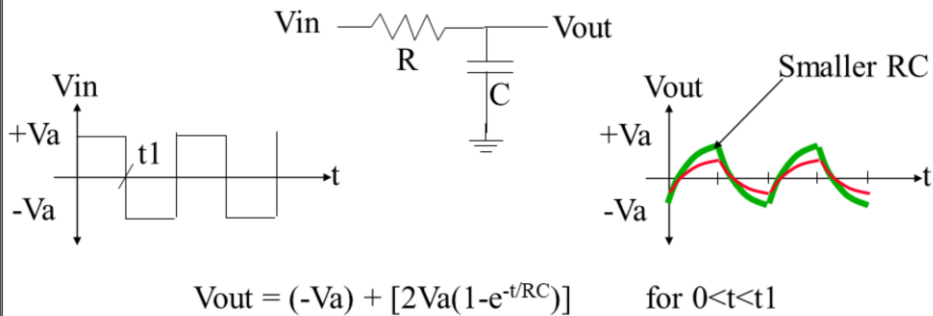
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Single resistors can be used to sense temperature, light, strain and are used in pressure sensors, accelerometers and other applications. With a dual supply op amp a small change in resistance can be converted to a change in voltage with a circuit such as the dual supply op amp circuit shown above. Initially $R1$ and $R2$ are identical and vin is zero. If the sensor resistor $R1$ increases in response to some physical change vin will decrease slightly. The amplifier has a gain of $\text{Gain} = 1 + (R3/R4)$ with infinite input resistance. $Vout$ will be a DC voltage relative to ground or zero volts.



This is an example of the non linear operation of an op amp because there is no feedback from output to the inverting input. Because of the high gain of the op amp any small difference in V_{in} compared to V_{ref} will be amplified by the huge gain of the op amp. So the output will be either $+V$ or $-V$ depending on if V_{in} is less than or greater than V_{ref} . The v_{out} vs v_{in} plot is shown for V_{in} swept from $-V$ to $+V$. The V_{out} will be $+V$ when V_{in} is less than V_{ref} and $-V$ when V_{in} is greater than V_{ref} .

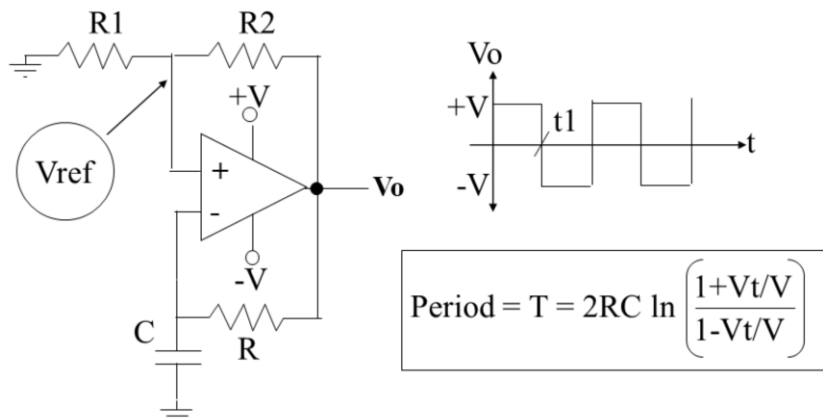
RC INTEGRATOR

If $R = 1\text{ MEG}$ and $C = 10\text{ pF}$ find $RC = 10\text{ us}$
 so t_1 might be $\sim 20\text{ us}$

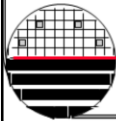


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Instead of sweeping the input let's use a RC circuit to charge a capacitor to whatever the output voltage is at. If the output voltage is high the capacitor will try to charge up to high. If the RC circuit is used with the comparator circuit discussed on the previous page the output voltage will switch to low when the capacitor voltage reaches V_{ref} making the output low and the capacitor will try to discharge to low but before it gets to $-V$ it reaches the V_{ref} Low and the output switches to high..... Thus continually oscillating high and low depending on the RC time constant.

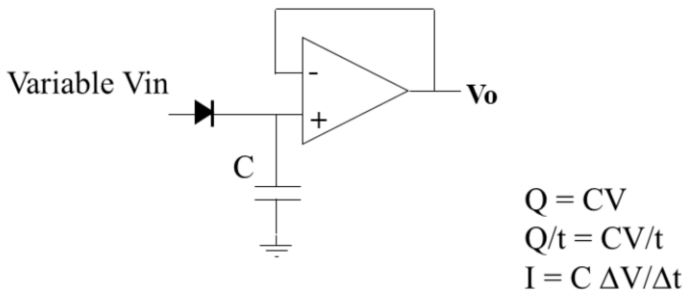
OSCILLATOR (MULTIVIBRATOR)

Bistable Circuit with Hysteresis and RC Integrator



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The voltage across the capacitor charges from $-V_{ref}$ towards $+V$ with time constant RC at $+V_{ref}$ it triggers and changes to charge toward $-V$ with time constant RC and continues to oscillate.

PEAK DETECTOR

Diode reverse leakage current, $I_s \sim 10\text{nA}$



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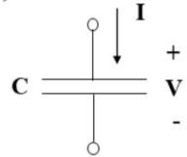
A changing input voltage will charge up the capacitor C to the peak of V_{in} . The capacitor will slowly discharge backwards through the diode with a constant current equal to the reverse leakage current, I_s . The equation shown can be used to calculate the change in voltage on a capacitor when it is being discharged with a constant current. For example if $I_s = 10\text{nA}$ and $C = 1\mu\text{F}$ the voltage across the capacitor can decrease at 10 millivolt per second. Adjusting the value of C changes how quickly V_{out} can respond to changes in V_{in} .

CAPACITORS AND CAPACITOR SENSORS

Capacitor - a two terminal device whose current is proportional to the time rate of change of the applied voltage;

$$I = dQ/dt = d(CV)/dt$$

$$= C dV/dt \text{ if } C \text{ is constant}$$



a capacitor C is constructed of any two conductors separated by an insulator. The capacitance of such a structure is:

$$C = \epsilon_0 \epsilon_r \text{Area}/d$$

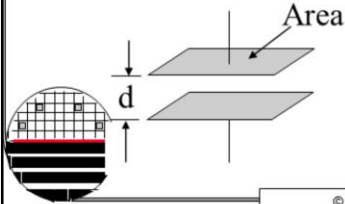
where ϵ_0 is the permittivity of free space
 ϵ_r is the relative permittivity
 Area is the overlap area of the two conductors separated by distance d

$$\epsilon_0 = 8.85 \times 10^{-14} \text{ F/cm}$$

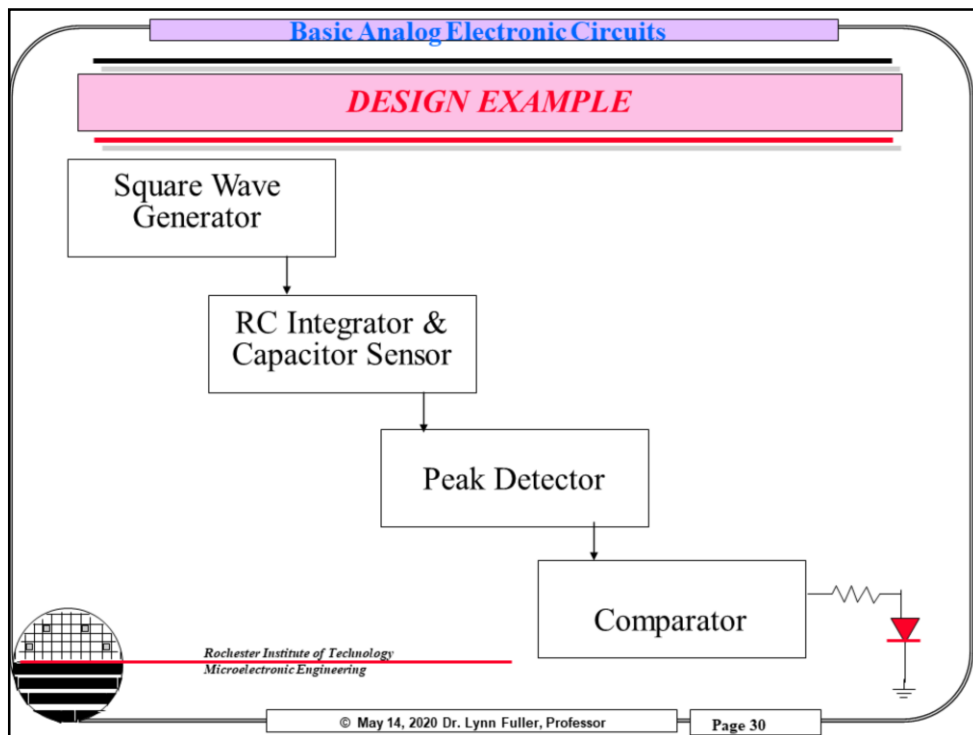
$$\epsilon_r \text{ air} = 1, \epsilon_r \text{ SiO}_2 = 3.9$$

$$\epsilon_r \text{ Si} = 11.7, \epsilon_r \text{ water} = 80$$

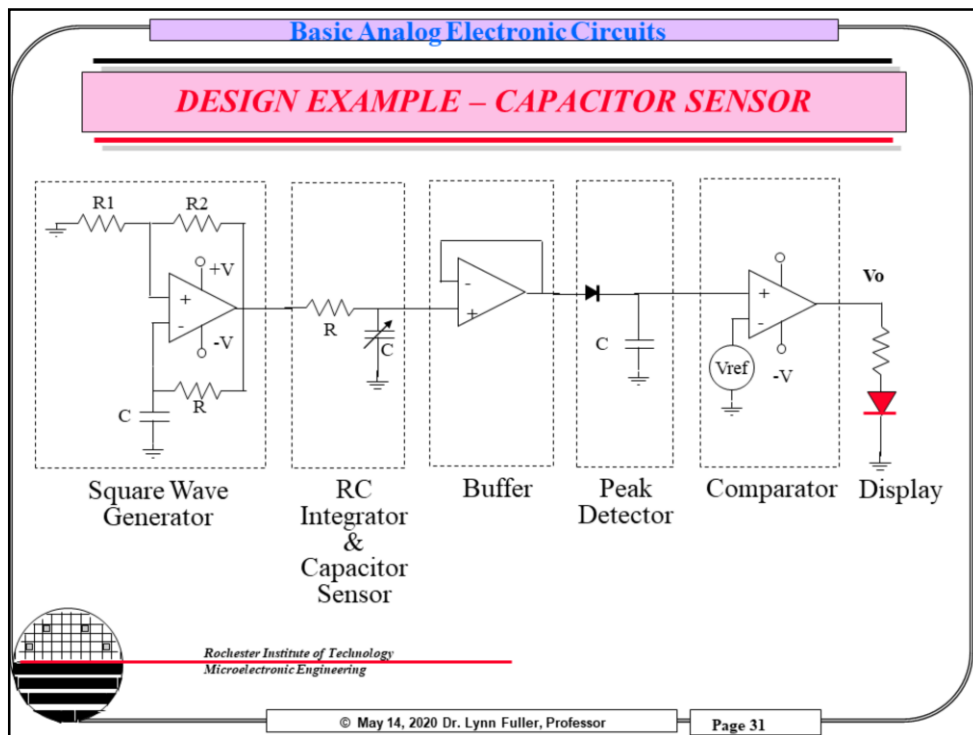
$$\epsilon_r \text{ rubber} = 3$$



The equations at the top show the relationship for voltage and current in a capacitor. The equation in the box can be used to calculate the capacitance for two parallel plates. Other conductor configurations have different equations for capacitance.

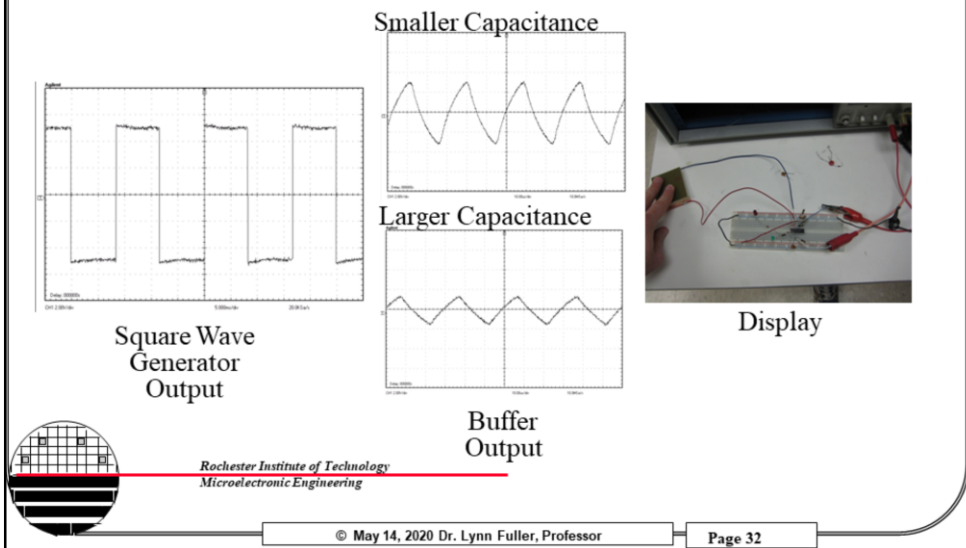


This shows an approach for an analog circuit design that will indicate when a capacitor sensor has reached some value. For example a capacitor used to measure a liquid level and when full turn on an LED indicator. Each block in the design approach above is converted into a circuit schematic on the next page.

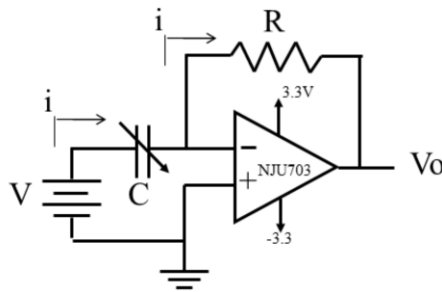


This shows the op amps and other components used to realize the capacitor sensor design.

EXAMPLE LABORATORY RESULTS



The circuit design from the previous page was used with a capacitor force sensor. Two parallel plates with foam between the plates. Pressure can push the plates closer increasing the capacitance. The buffer output shows that the waveform peak is related to the capacitance value. A bread board for this circuit was built and the signals were obtained using an oscilloscope. Note: this type of circuit can detect slowly changing capacitance values or even different steady capacitance values.

CAPACITOR MICROPHONE PLUS AMPLIFIER

$$V_o = -i R$$

$$i = d(CV)/dt, V \text{ is constant } C = C_0 + C_m \sin(2\pi ft)$$

$$i = V dC/dt$$

$$i = V C_m 2\pi f \cos(2\pi ft)$$

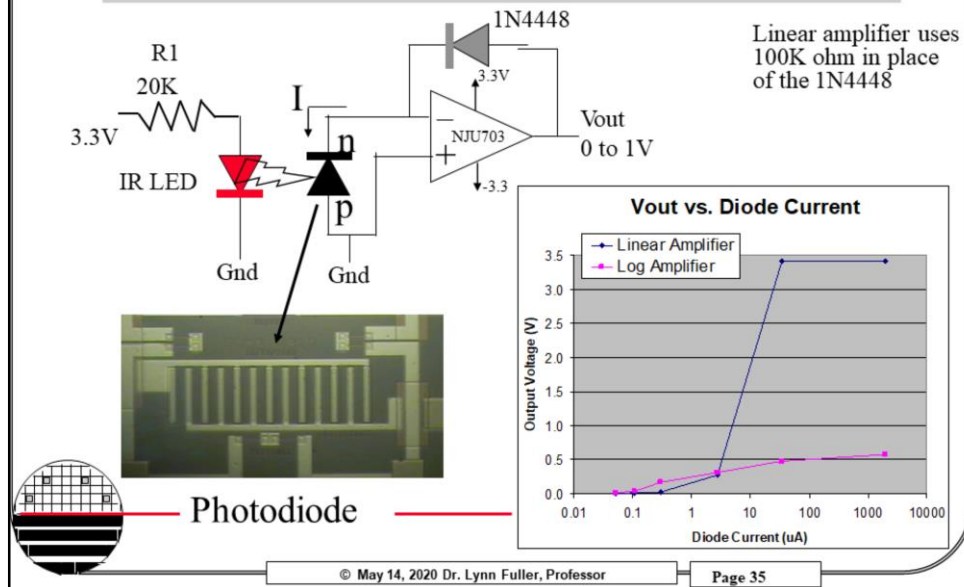


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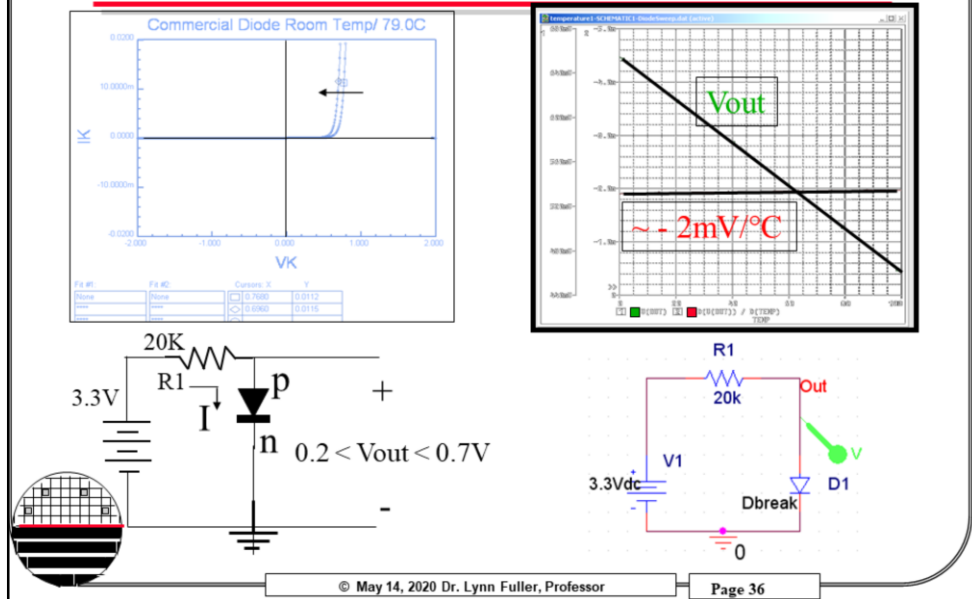
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Microphones have a capacitor sensor that changes with sound pressures. The capacitor is a thin flexible diaphragm parallel plate structure. A small microphone, like the one in your smart phone, might have a capacitance of several pF with changes in capacitance of a few hundred fF in response to sound pressure waves. The capacitance changes will be at audio frequencies, say 1KHz to 10KHz range. The capacitance is shown as $C_0 + C_m \sin(2\pi ft)$ where C_0 might be 10pF and C_m might be 100fF and the frequency might be 5KHz. The calculation for V_o is shown in this slide. Do the math and find the amplitude of the output voltage for R of 1MEG. This circuit converts changing capacitance to changing voltage.

PHOTO DIODE I TO V LOG AMPLIFIER

Light intensity changes many orders of magnitude from dark to very bright. A non linear current to voltage converter is shown here where the feedback resistor is replaced with a diode. The plot shows the difference between a linear amplifier, R in feedback, and logarithmic amplifier, diode in feedback, for photo diode currents over many orders of magnitude. This could be useful to set the exposure time for a camera based on the brightness.

SIGNAL CONDITIONING FOR TEMPERATURE SENSOR



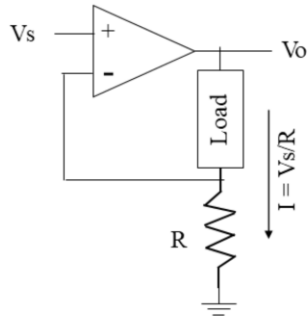
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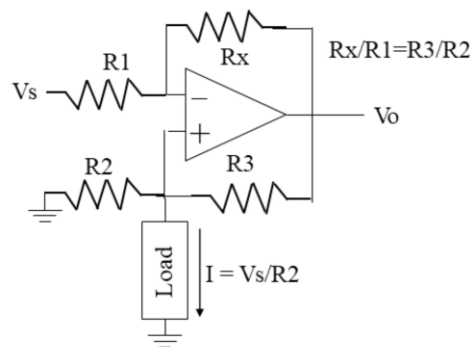
The forward voltage drop across a forward biased diode changes by $\sim -2\text{mV}/^\circ\text{C}$. This circuit forward biases a diode operating at approximately $(3.3 - 0)/20\text{K} = 0.13\text{ mA}$. The plot of V_{out} has a slope of $\sim -2\text{mV}/^\circ\text{C}$ which is fairly constant over the temperature range shown on the x-axis of zero to 100°C . The I-V curve shifts to the left at higher temperatures.

OP AMP CONSTANT CURRENT SOURCE

Floating Load

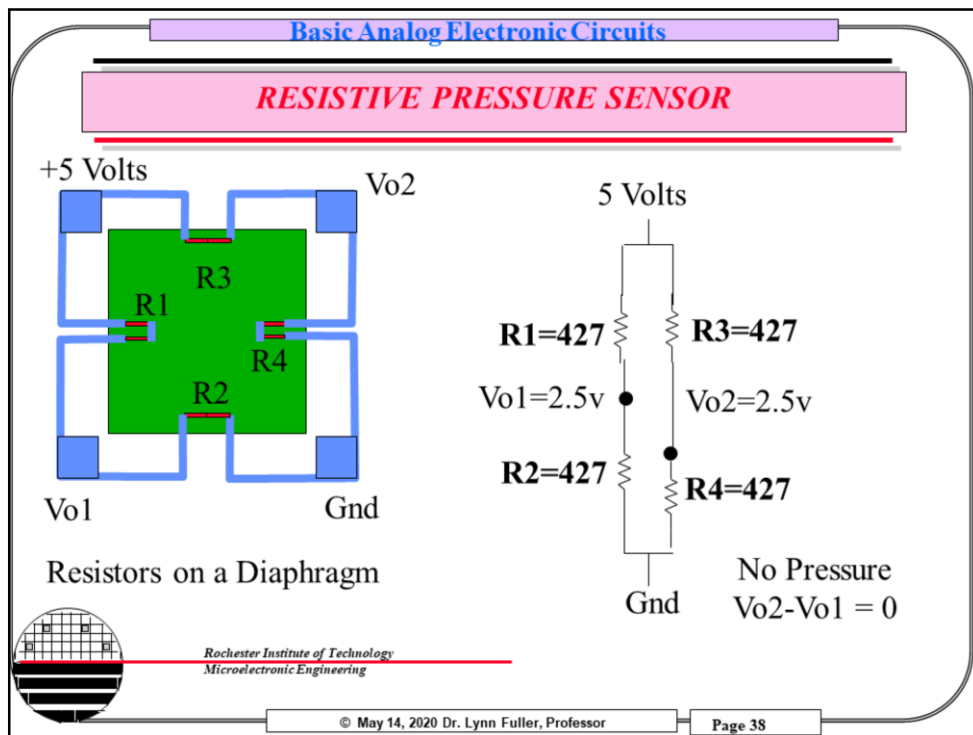


Grounded Load

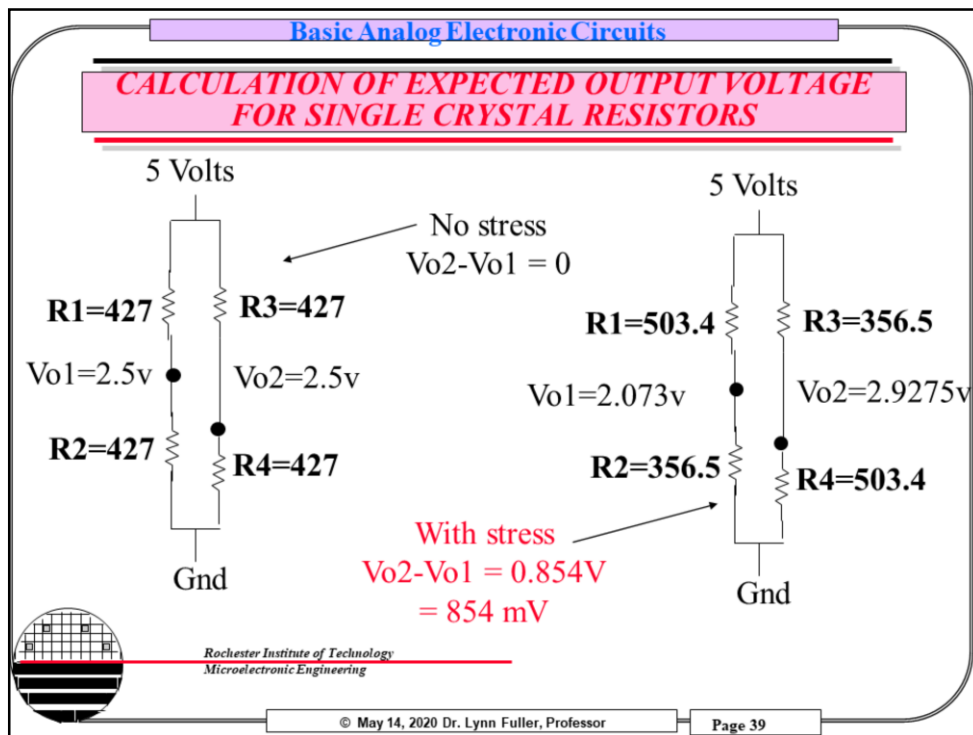


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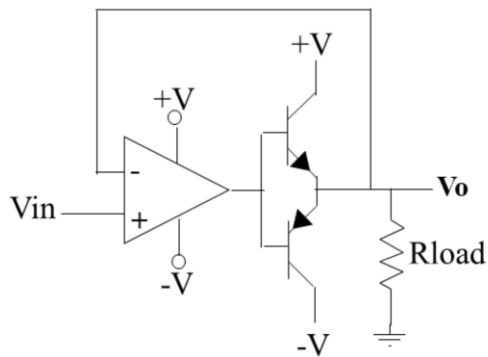
These two circuits provide a constant current to the load. The current value is set by the voltage V_s .



This figure shows four resistors on a diaphragm use for sensing pressure. With no pressure all the resistors are equal in value. When pressure is applied a stress occurs making R1 and R4 longer and making R3 and R2 wider. The resistors change a little with pressure. How much they change depends on the how the resistors are made. In general the could by resistors in single crystal silicon or thin film resistors on top of the diaphragm. P-type resistors in single crystal silicon with a specific crystal orientation would result in R1 and R4 increasing in resistance while R3 and R2 decrease in resistance. See the next page.



This is a possible comparison of resistor values with no pressure applied on the left and with a specific amount of pressure applied on the right. V_{o2} increases and V_{o1} decreases. The pressure sensors in your smart phone work like this.

POWER OUTPUT STAGE

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Op amps have limited output current. If you want a little more output current you can use power transistors as shown to boost the current available to the load. This is a unity gain configuration with infinite input resistance and voltage gain of 1 V/V

REFERENCES

1. Switched Capacitor Circuits, Phillip E. Allen and Edgar Sanchez-Sinencio, Van Nostrand Reinhold Publishers, 1984.
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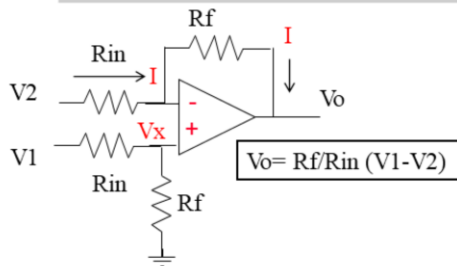
HOMEWORK – BASIC ANALOG CIRCUITS

1. Design a bistable multivibrator with V_{th} of ± 7.5 volts and frequency of 5 KHz.
2. Design a temperature sensor circuit that will shut down a heater if the temperature exceeds 90°C
3. Design a peak detector that will respond to changes in input in less than one second.
4. Derive the voltage gain equation for the difference amplifier.



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DERIVE GAIN EQUATION FOR DIFFERENCE AMP



$$I = (V2 - V_x)/R_{in}$$

$$V_x = V1 \frac{R_f}{R_f + R_{in}}$$

$$V_o = -I R_f + V_x$$

Difference Amplifier



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